



Aerospace Combustion

Lecture 5:

Combustion: Basic Definitions and Equations Part 2



Content



- Standard Entropy and Enthalpy
- Chemical Potential and Chemical Equilibrium
- Propellant Mixtures
- Standard Enthalpy and Entropy and Changes
- Gibbs and Helmholtz Energies
- Fugacity

Standard Entropy

- Standard means at standard pressure (1 atm) and temperature (298 K)
- Values can be found in the literature for almost any substance
- Entropy is an extensive property (function of the number of moles)
- The more complex the molecule, the higher the standard entropy value
- Literature provides data for almost any substance

Element	S°_{298}	Compound	S°_{298}
$H_2(g)$	131	$H_2O(l)$	70
$O_2(g)$	205	$H_2O(g)$	189
$N_2(g)$	193	$H_2O_2(g)$	110
$Cl_2(g)$	223	$N_2O_4(g)$	304
$He(g)$	126	$NH_3(g)$	192
$Ne(g)$	146	$NaCl(s)$	72
$C(s, \text{diamond})$	2.4	$NaCl(aq)$	116
$C(s, \text{graphite})$	5.7	$CH_4(g)$	186
$S(s)$	32	$CO_2(g)$	213

Some Standard Molar Entropy Values at 298.15 K*

Compound or Element	Entropy, $S^\circ(\text{J/K}\cdot\text{mol})$	Compound or Element	Entropy, $S^\circ(\text{J/K}\cdot\text{mol})$	Compound or Element	Entropy, $S^\circ(\text{J/K}\cdot\text{mol})$
C(graphite)	5.740	Ar(g)	154.7	$Cl_2(g)$	223.036
C(g)	158.096	$H_2(g)$	130.684	$Br_2(l)$	152.2
$CH_4(g)$	186.64	$O_2(g)$	205.138	$I_2(s)$	116.135
$C_2H_6(g)$	229.60	$N_2(g)$	191.61	$NaCl(s)$	72.8
$C_3H_8(g)$	269.9	$H_2O(g)$	188.825	$NaF(s)$	51.5
$CH_3OH(l)$	126.8	$H_2O(l)$	69.91	$MgO(s)$	26.94
$CO(g)$	197.674	$NH_3(g)$	192.45	$MgCO_3(s)$	65.854
$CO_2(g)$	213.74	$HCl(g)$	186.908		
Ca(s)	41.42	$F_2(g)$	202.78		

Taken from "The NBS Tables of Chemical Thermodynamic Properties," 1982.

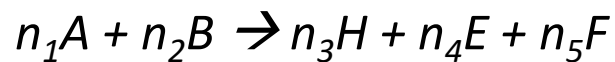
Entropy Change in a Reaction

Using standard molar entropies you are able to predict the entropy change of reactions

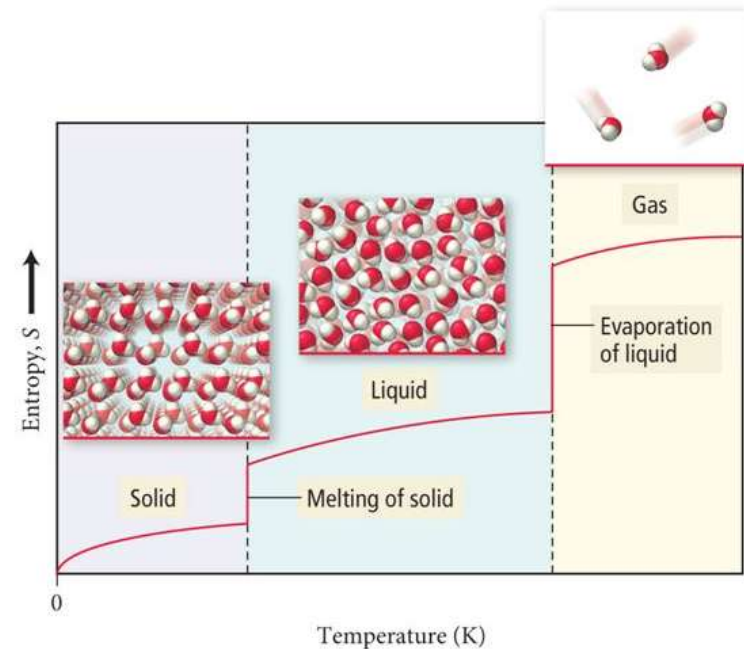
$$\Delta S = \sum n_p S_{products}^0 - \sum n_r S_{reactants}^0$$

Phase changes lead to entropy changes which is important since propellants generally enter in liquid state and the products are gaseous.

Example:

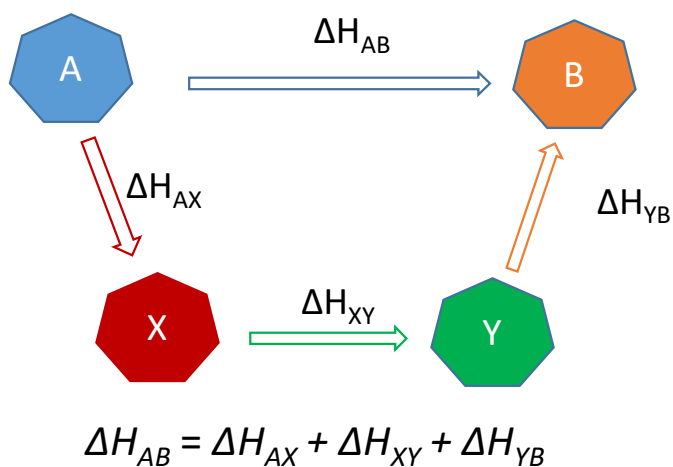


$$\Delta S = [n_3 S_H^0 + n_4 S_E^0 + n_5 S_F^0] - [n_1 S_A^0 + n_2 S_B^0]$$

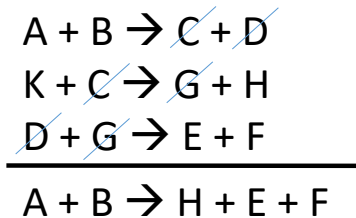


Enthalpy of Formation

Law of Hess: “The *sum* of the enthalpy changes for a number of individual reaction steps equals the enthalpy change of the overall reaction.



This holds even for larger and more complex systems

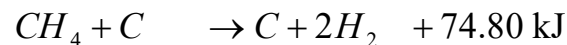
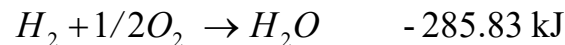
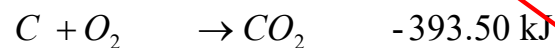
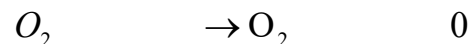


Step 1: elements \rightarrow reactants provides $\Delta H_{\text{reactants}}$

Step 2: elements \rightarrow products provides $\Delta H_{\text{products}}$

Step 3: $\Delta H_{\text{reaction}} = \Delta H_{\text{reactants}} + \Delta H_{\text{products}}$

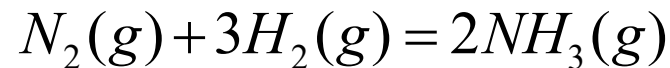
Combustion of methane $CH_4 + 2O_2 \rightarrow CO_2 + 2H_2O$



- Formation of an element from an element is **Zero**.
- The reactants have to appear on the left side of the equation.

Example

Let's predict the standard entropy of the formation reaction of ammonia from the elements at standard conditions



$$\begin{aligned}\Delta S^0 &= 2S^0(NH_3) - [S^0(N_2) + 3S^0(H_2)] \\ &= (2 \text{ mol}) \left(192.3 \frac{J}{K \cdot mol} \right) - \left[(1 \text{ mol}) \left(191.5 \frac{J}{K \cdot mol} \right) + (3 \text{ mol}) \left(130.6 \frac{J}{K \cdot mol} \right) \right] \\ &= -198.7 \frac{J}{K}\end{aligned}$$

The formation entropy is negative since the reaction reduces the number of moles from **four** to **two**.

Chemical Reactions

Literature provides Data for ΔG° , ΔH° , S° , and c_p°

@ 1 bar, 298K	M/ (g/mol)	$\Delta_f \bar{H}^\circ / (kJmol^{-1})$	$\Delta_f \bar{G}^\circ / (kJmol^{-1})$	$\bar{S}^\circ / (Jmol^{-1}K^{-1})$	$\bar{c}_p^\circ / (Jmol^{-1}K^{-1})$
H ₂ (g)	2.016	0	0	130.684	28.824
H (g)	1.008	217.97	203.25	114.71	20.784
H ⁺ (aq)	1.008	0	0	0	0
H ⁺ (g)	1.008	1536.20			
H ₂ O (s)	18.015			37.99	
H ₂ O (l)	18.015	-285.83	-237.13	69.91	75.291
H ₂ O (g)	18.015	-241.82	-228.57	188.83	33.58
H ₂ O ₂ (l)	34.015	-187.78	-120.35	109.6	89.1
O ₂ (g)	31.999	0	0	205.138	29.355
O (g)	15.999	249.17	231.73	161.06	21.912
O ₃ (g)	47.998	142.7	163.2	238.93	39.20
HO ⁻ (aq)	17.007	-229.99	-157.24	-10.75	-148.5



Chemical Equilibrium

Chemical equilibrium accounts for impact of pressure and temperature on the formation of reaction products

- Does not hold for slow chemical reactions, typically low temperatures where in the residence time of the propellants in the control volume won't reach equilibrium
- Such cases finite rate kinetic mechanisms
- Chemical equilibrium represents exact thermodynamic limit

Chemical Potential

Chemical potential is equivalent to the partial molar free Gibbs energy



Equilibrium Constants

Several ways to predict equilibrium constants

Use chemical potentials and apply

- Enthalpies of formation
- Entropies of formation
- Specific heats

Use an approximation approach by neglecting temperature dependency of specific heat

Chemical Equilibrium, Chemical Potential

Partial molar entropy of chemical species in an ideal gas mixture

$$s_{i,m} = s^0_{i,m} - R \ln\left(\frac{p_i}{p_0}\right); i = 1, 2, \dots, k$$

with $p_0 = 1 \text{ atm}$

and

$$s^0_{i,m} = s^0_{i,m,ref} + \int_{T_{ref}}^T \frac{c_{p,i,m}}{T} dT; i = 1, 2, \dots, k$$

and which depends only on temperature. Values for these are listed in tables.

The constant pressure heat capacity is a function of the temperature only and is usually represented by a power series in T .

$$c_p = a_0 + a_1T + a_2T^2 - a_3T^3 + \dots$$

Chemical Equilibrium, Chemical Potential

Free Gibbs energy for mixtures

$$G = \sum_{i=1}^n n_i g_{i,m};$$

Equilibrium is reached when Gibbs free energy is minimum,
 i.e. $dG = 0$

$$dG = Vdp - sdT + \sum_{i=1}^N \mu_i dn_i;$$

from total differential $dG = \frac{\partial G}{\partial p} \Big|_{T, \{n_i\}} dp + \frac{\partial G}{\partial T} \Big|_{p, \{n_i\}} dT + \sum_{i=1}^N \frac{\partial G}{\partial p} \Big|_{T, p, \{n_{j,i \neq j}\}} dn_i;$

follows $\frac{\partial G}{\partial p} \Big|_{T, p, \{n_{j,i \neq j}\}} = \mu_i$ and since $G = \sum_{i=1}^n n_i g_{i,m};$

$\rightarrow \mu_i = g_{i,m}$
 Chemical potential is equivalent to the partial molar free Gibbs energy

Prediction of Equilibrium Constant

Generally an equilibrium constant can be predicted using the stoichiometric coefficients and the chemical potential of the species in question and the latter depends on their enthalpies and entropies of formation and their specific heats

$$K_p(T) = \exp\left(\sum_{i=1}^n \frac{\nu_i \mu_i^0}{RT}\right)$$

with

$$\frac{\mu_i^0}{RT} = \frac{h_{i,m_{ref}}}{RT} - \frac{s_{ref}}{R} + \frac{1}{RT} \int c_{p_i} dT + \int \frac{c_p}{RT} dT$$

Approximation of Equilibrium Constants

For constant specific heats c_{p_i}

the approximate solution

$$K_p(T) = \exp\left(\frac{-\sum_{i=1}^n \nu_i h_{i,m,ref}}{RT}\right) \underbrace{\exp\left(\sum_{i=1}^n \nu_i S_{ref} / R\right)}_{\text{constant}} \underbrace{\exp\left(\sum_{i=1}^n \nu_i c_{p_i} \frac{T - T_{ref}}{RT}\right)}_{\approx \text{constant}} \underbrace{\exp\left(\sum_{i=1}^n \nu_i \frac{c_{p_i}}{R} \ln\left(\frac{T}{T_{ref}}\right)\right)}_{\approx \exp(n \ln T)}$$

finally reads:

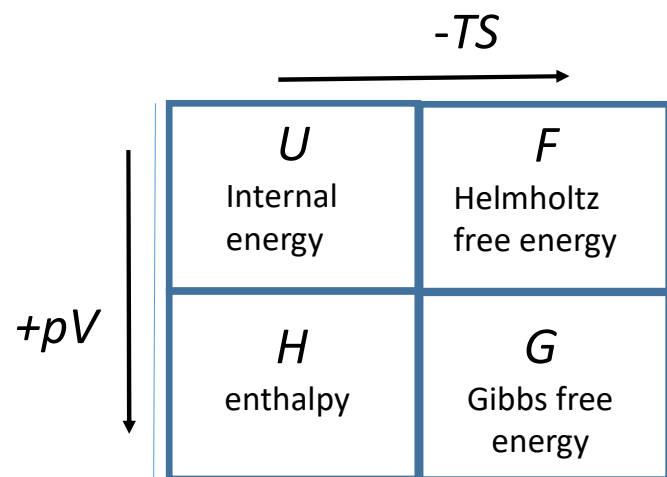
$$K_p(T) = \exp\left(\frac{-\Delta h_{m,ref}}{RT}\right) \exp\left(\sum_{i=1}^n \nu_i \pi_{i,A}\right) \exp\left(\sum_{i=1}^n \nu_i \pi_{i,B} \ln(T)\right)$$

* Values for $\pi_{i,A}$ and $\pi_{i,B}$ for some species can be found in the annex

Gibbs free Energy

$$\Delta G^0 = \Delta H^0 - TdS^0$$

- Allows to calculate maximum non-expansive, reversible work that can be performed by a thermodynamic system at constant (p,T)
- For a system is at equilibrium at (p,T constant) the free Gibb's energy is a its minimum



Not to be mixed with
Helmholtz free Energy

$$F = U - TS$$

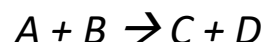
- Allows to calculate the useful work obtainable from a closed system at constant temperature and volume
- F is quite often used in explosives research where pressure changes come naturally.

The four thermodynamic potentials U , F , H , and G are related by offsets of the energy from the environment term TS and the expansion work term pV .



Equilibrium Constant

Let's look at the reaction



and formulate this in terms of free Gibbs energy

with $\Delta G = 0$

$$G_A = G_A^0 + aRT \ln(p_A)$$

$$G_B = G_B^0 + bRT \ln(p_B)$$

$$G_C = G_C^0 + cRT \ln(p_C)$$

$$G_D = G_D^0 + dRT \ln(p_D)$$

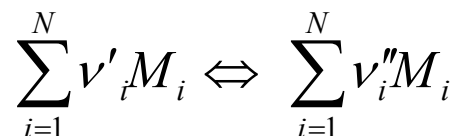
$$\Delta G = G_{prod} - G_{react}$$

$$= \Delta G^0 + RT \ln \left(\frac{p_C^c p_D^d}{p_A^a p_B^b} \right)$$

$$\Delta G^0 = -RT \ln \left(\frac{p_C^c p_D^d}{p_A^a p_B^b} \right) = RT \ln K_p$$

Large negative values of ΔG^0 are mainly due to large **equilibrium constant K_p** which means that the reaction is faster. In case the free energy of reactants and products are the same, there will be no progress of the reaction and $\Delta G = 0$.

A general reaction of the form



yields such an equilibrium constant

$$K_p = \prod_{i=1}^N (p_{i,e})^{(\nu''_i - \nu'_i)}$$

Various Equilibrium Constant Formulations

$$K_p = \prod_{i=1}^N (p_{i,e})^{(v''_{i,s} - v'_{i,s})}$$

$$K_n = \prod_{i=1}^N (n_{i,e})^{(v''_{i,s} - v'_{i,s})}$$

$$K_c = \prod_{i=1}^N (c_{i,e})^{(v''_{i,s} - v'_{i,s})}$$

$$K_X = \prod_{i=1}^N (X_{i,e})^{(v''_{i,s} - v'_{i,s})}$$

$$K_Y = \prod_{i=1}^N (Y_{i,e})^{(v''_{i,s} - v'_{i,s})}$$

$$c_i = \frac{p_i}{RT}$$

$$n_i = \frac{p_i V}{RT} = \frac{p_i}{p} n_T$$

$$X_i = \frac{p_i}{p} = \frac{n_i}{n_T}$$

$$Y_i = \frac{W_i p_i}{\rho RT} = \frac{W_i c_i}{\rho} = \frac{\rho_i}{\rho}$$

$$n_T = \sum_{i=1}^N n_i$$

$$p = \sum_{i=1}^N p_i$$

$$\rho$$

Concentration of species i

actual number of moles of species i

mole fraction of species i

Mass fraction of species i

Total number of moles in mixture

Total mixture pressure

Mixture density

Interrelation of Various Formulations

$$\begin{aligned}
 K_p &= K_c (RT)^{\Delta n} = \\
 &= K_n \left(\frac{p}{n_T} \right)^{\Delta n} = \\
 &= K_X (p)^{\Delta n} = \\
 &= K_Y (RT\rho)^{\Delta n} \prod_{i=1}^N (W_i)^{(v'_{i,s} - v''_{i,s})}
 \end{aligned}$$

for cases where

$$\Delta n = \sum_{i=1}^N \nu_i'' - \sum_{i=1}^N \nu_i' \neq 0$$

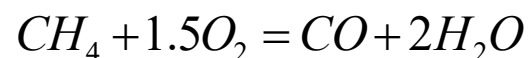
then K_p is a function of temperature only,

all others are functions of pressure and temperature

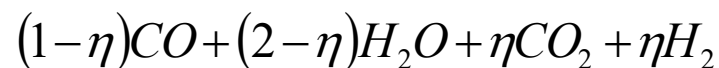


Example 1:

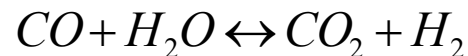
Let's consider the reaction of methane with oxygen to form carbon-monoxide and water



Quite often at high temperatures the chemical equilibrium may look like



due to a reaction called water-gas reaction



Question: Write the necessary mathematical relationships required to solve the equilibrium composition

Example 1:

K_p for the water-gas reaction reads

$$K_p = \frac{p_{CO_2} p_{H_2}}{p_{CO} p_{H_2O}} \quad n_T = \sum_{i=1}^N n_i = (1-\eta) + (2-\eta) + \eta + \eta = 3$$

$$\rightarrow X_{CO} = \frac{1-\eta}{3}; X_{H_2O} = \frac{2-\eta}{3}; X_{CO_2} = \frac{\eta}{3} = X_{H_2};$$

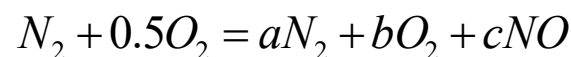
$$\rightarrow p_{CO} = \frac{1-\eta}{3} p; p_{H_2O} = \frac{2-\eta}{3} p; p_{CO_2} = \frac{\eta}{3} p = p_{H_2};$$

$$\rightarrow K_p = \frac{p_{CO_2} p_{H_2}}{p_{CO} p_{H_2O}} = \frac{\left(\frac{\eta}{3}\right)^2 p^2}{\left(\frac{1-\eta}{3}\right) p \left(\frac{2-\eta}{3}\right) p} = \frac{\eta^2}{(1-\eta)(2-\eta)}$$



Example 2:

Let's heat 1 mole of nitrogen and 0.5 mole of oxygen to 4000 K at 1 bar and consider an equilibrium composition of N_2 , O_2 and NO only.



Question: What is the final equilibrium composition?

$$N: 2 = 2a + c$$

$$O: 1 = 2b + c$$

Conservation of atoms yields:

$$a = 1 - \frac{c}{2}; b = \frac{1}{2} - \frac{c}{2}$$

From tables we know that $K_p \sim 0.3$:

$$K_p = \frac{p_{NO}}{p_{N_2} p_{O_2}} = \frac{x}{(1 - x/2)^{1/2} (1/2 - x/2)^{1/2}} \left(\frac{p}{\sum n} \right)^{1-1/2-1/2} \Rightarrow 0.09 = \frac{x^2}{(1 - x/2)(1/2 - x/2)} \Rightarrow x = 0.1825$$

Final mixture composition is then: $0.90875N_2 + 0.40875O_2 + 0.1825NO$



Fugacity (f)

Fugacity is a quantity which represents the actual behavior of real gases

For ideal gases at constant temperature

$$dG = nRTd (\ln p)$$

for non-ideal gases

$$dG = nRTd (\ln f)$$

Fugacity may be considered a correction to the partial pressure

The proportionality constant Γ is a function of many parameters such as temperature and pressure

$$f_i = p_i \Gamma (p, T, \dots)$$

For an ideal gas

$$\frac{f_i}{p_i} = 1$$



Fugacity (f)

For decreasing pressure real gases approach ideal gas behavior

Assuming an isothermal process at temperature T , the fugacity f can be determined from the compressibility factor Z and the pressure p by

Integration at constant T from $p = 0$ to a certain finite pressure p yields

The right hand side is accessible from compressibility charts, see next page

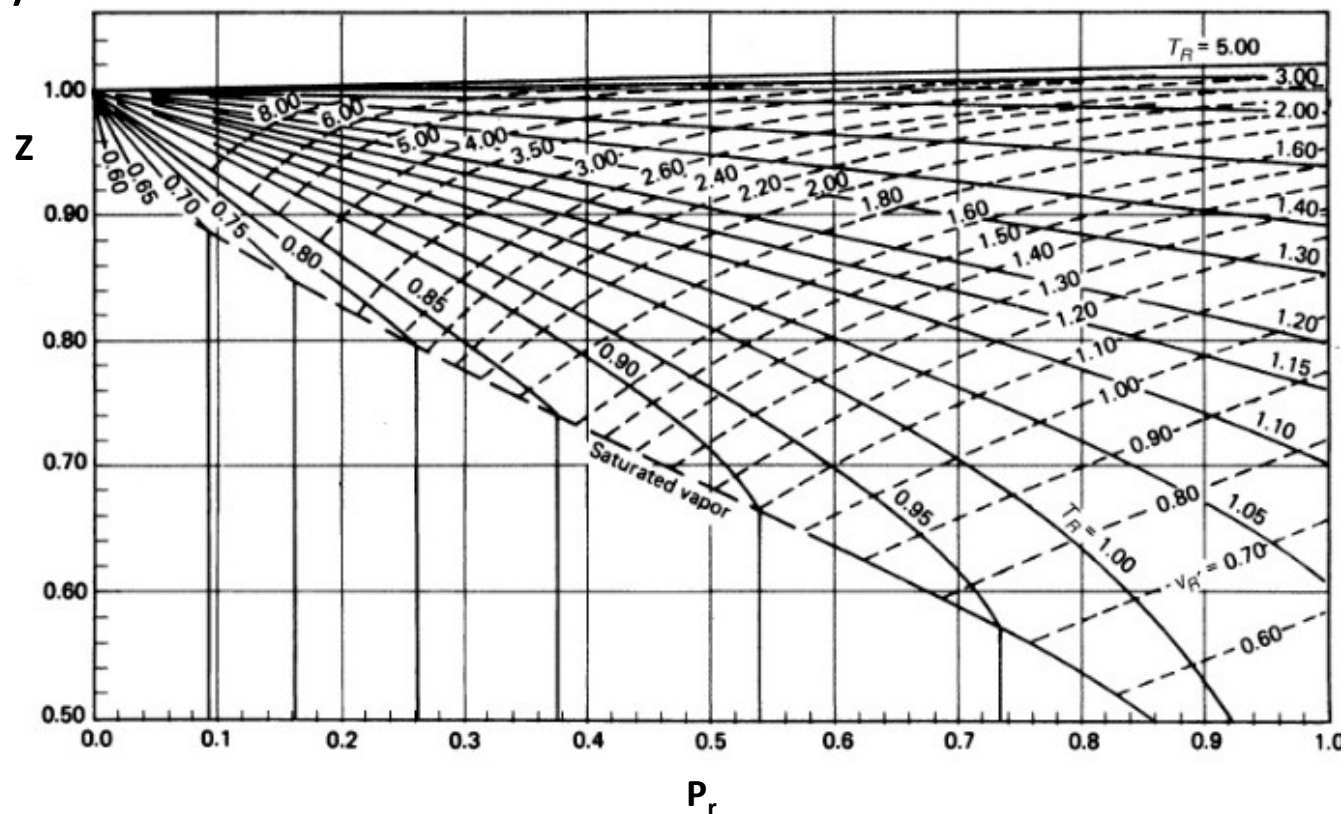
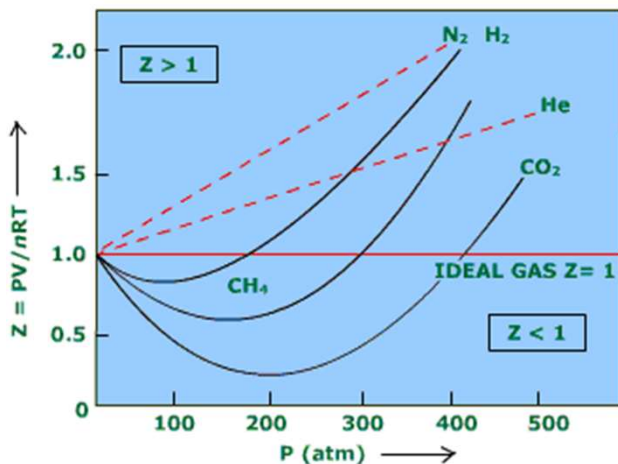
$$\lim_{p \rightarrow 0} \left(\frac{f}{p} \right) = 1$$

$$Z d(\ln p)_T = d(\ln f)_T$$

$$\ln \frac{f}{p} = \int_0^p (Z - 1) d(\ln p_r)_T$$

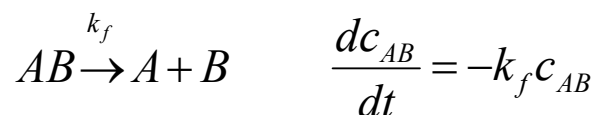
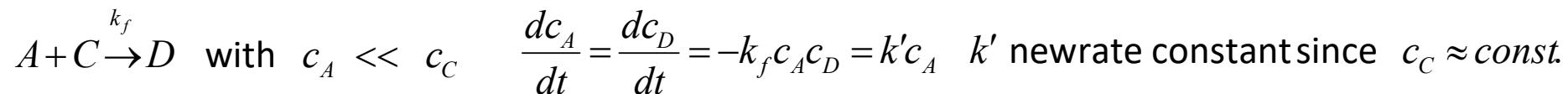
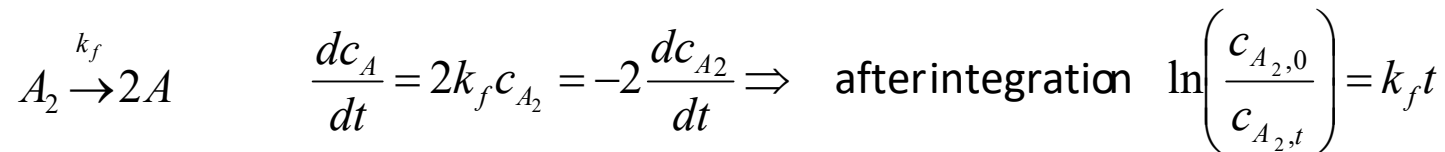
Generalized Compressibility Chart

Such charts are available for almost any common species



Order of Sample Reactions

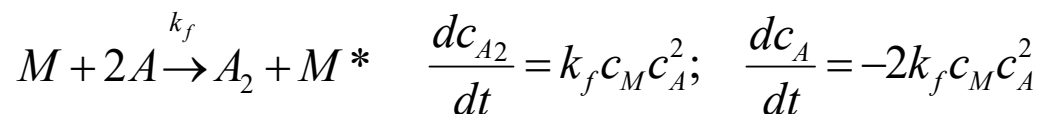
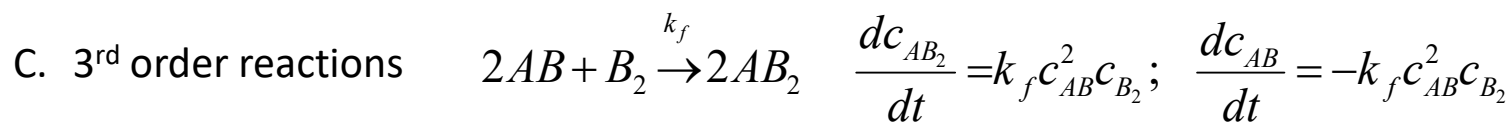
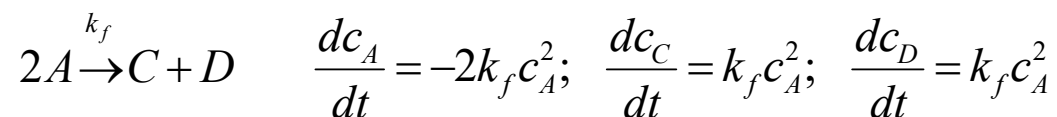
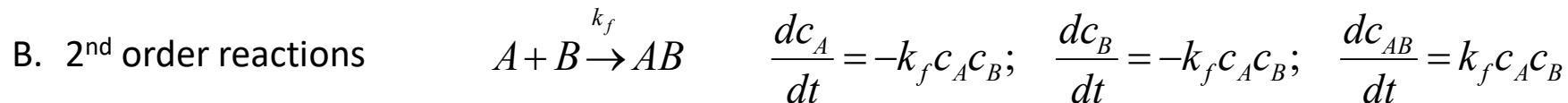
A) 1st order reactions



While the decomposition of A₂ is a uni-molecular reaction which obeys first order kinetics, the formation of D out of A+B is a bi-molecular reaction which again obeys first order kinetics.

→ Uni-molecular reactions are always first order but not all first order reactions are mono-molecular.

Order of Sample Reactions



Order of Sample Reactions

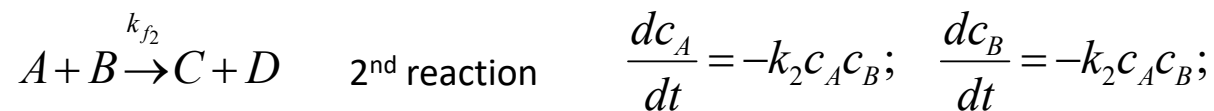
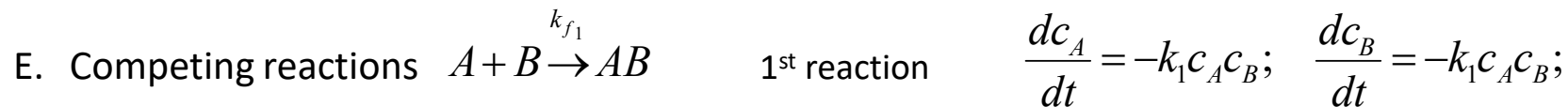


1st reaction $\frac{dc_{AB}}{dt} = k_1 c_A c_B; \quad \frac{dc_A}{dt} = \frac{dc_B}{dt} = -k_1 c_A c_B;$

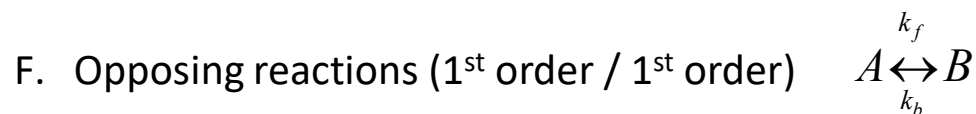
2nd reaction $\frac{dc_{AB}}{dt} = k_2 c_{AB}; \quad \frac{dc_C}{dt} = \frac{dc_D}{dt} = -k_2 c_{AB};$

net reaction $\left(\frac{dc_{AB}}{dt} \right)_{net} = k_1 c_A c_B - k_2 c_{AB};$

Order of Sample Reactions



Quite often competing reaction may have different rates depending on temperature.



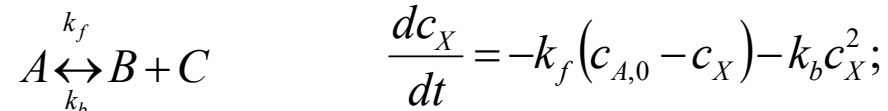
Note c_X is the portion of A converted to B by the forward reaction with $c_{A,0}$ the initial concentration

$$c_A = c_{A,0} - c_X; \quad \frac{dc_X}{dt} = k_f (c_{A,0} - c_X) - k_b c_X;$$

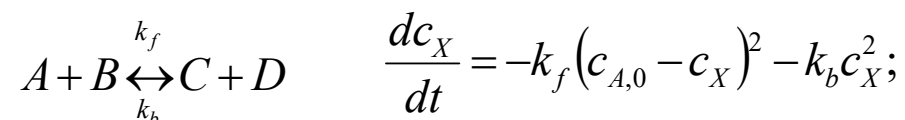
$$c_B = c_X; \quad c_{B,0} = 0$$

Order of Sample Reactions

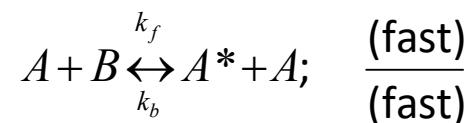
G. Opposing reactions (1st order / 2nd order)



H. Opposing reaction (2nd order / 2nd order)



I. Chain reaction (formation of radical)



According to Lindemann only a small portion of molecules will become energized by collisions A^* and as long as their conversion rate into products is small the following relations hold.

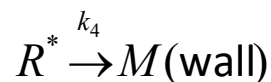
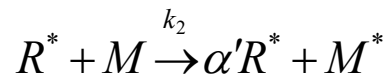
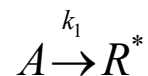
$$\frac{dc_A}{dt} = k_f c_A^2 + k_b c_{A^*} c_A$$

$$\frac{dc_{A^*}}{dt} = k_f c_A^2 - k_b c_{A^*} c_A - k'_f c_{A^*};$$

Order of Sample Reactions

J. Chain branching reactions

General formulation of a chain-branching reaction



Assuming steady-state condition

$$\frac{dc_{R^*}}{dt} = 0 = k_1 c_M + (\alpha' - 1) k_2 c_{R^*} c_M - k_3 c_{R^*} c_{M^*} - k_4 c_{R^*} - k_5 c_{R^*}$$

$$\frac{dc_P}{dt} = k_3 c_{R^*} c_{M^*}$$

$$\alpha'_{crit} = 1 + \frac{k_3 c_{R^*} c_{M^*} + k_4 + k_5}{k_2 c_{M^*}}$$

if

$$\alpha' \geq \alpha'_{crit} \Rightarrow \text{chain - branching explosion}$$

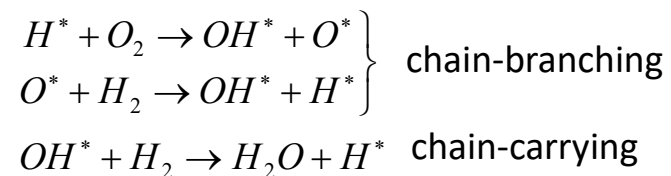
$$\alpha' \leq \alpha'_{crit} \Rightarrow \text{no explosion}$$



Order of Sample Reactions

J. Chain branching reactions

In a hydrogen oxygen mixture and in presence of an OH radical the following reaction cycle is plausible



Let's consider that the chain-carrying reaction is dominating and we have a volume of 1 cm^3 which contains roughly 10^{19} molecules and 1 radical. At a collision rate of 10^8 1/s it would take around 30000 years for all molecules to react.

Now let's assume that 1 radical is able to generate 2 radicals ($\alpha'=2$) then all molecules will react within about $1 \mu\text{s}$.

If we assume that only 1% of the reactions are chain-branching ($\alpha'=1.01$) this time increase to about $40 \mu\text{s}$.



What you should not forget

- Mole fraction, mass fraction, molar density,
- Mixture fraction, stoichiometric value, equivalence ratio
- Why a cubic equation of state combustion is often necessary
- Difference between global and elementary reactions
- Reaction rate
- Enthalpy, entropy at standard conditions and for formation
- Gibbs and Helmholtz energy
- Order of reactions
- Fugacity
- Chain reactions
- Explosions



Content

- Properties of common species in combustion
- Enthalpies and entropies of formation of common species
- Relations to predict fluid properties



Properties of Gases

		M_i [kg/kmol]	$h_{i,m,ref}$ [kJ/mol]	$s_{i,m,ref}$ [kJ/mol K]	$\pi_{A,i}$	$\pi_{B,i}$
1	H	1,008	217,986	114,470	-1,2261	1,9977
2	HNO	31,016	99,579	220,438	-1,0110	4,3160
3	OH	17,008	39,463	183,367	3,3965	2,9596
4	HO ₂	33,008	20,920	227,358	-,1510	4,3160
5	H ₂	2,016	0,000	130,423	-2,4889	2,8856
6	H ₂ O	18,016	-241,826	188,493	-1,6437	3,8228
7	H ₂ O ₂	34,016	-136,105	233,178	-8,4782	5,7218
8	N	14,008	472,645	153,054	5,8661	1,9977
9	NO	30,008	90,290	210,442	5,3476	3,1569
10	NO ₂	46,008	33,095	239,785	-1,1988	4,7106
11	N ₂	28,016	0,000	191,300	3,6670	3,0582
12	N ₂ O	44,016	82,048	219,777	-5,3523	4,9819



Properties of Gases

		M_i [kg/kmol]	$h_{i,m,ref}$ [kJ/mol]	$s_{i,m,ref}$ [kJ/mol K]	$\pi_{A,i}$	$\pi_{B,i}$
13	O	16,000	249,194	160,728	6,85561	1,9977
14	O ₂	32,000	0,000	204,848	4,1730	3,2309
15	O ₃	48,000	142,674	238,216	-3,3620	5,0313
16	NH	15,016	331,372	180,949	3,0865	2,9596
17	NH ₂	16,024	168,615	188,522	-1,9835	3,8721
18	NH ₃	17,032	-46,191	192,137	-8,2828	4,8833
19	N ₂ H ₂	30,032	212,965	218,362	-8,9795	5,4752
20	N ₂ H ₃	31,040	153,971	228,513	-17,5062	6,9796
21	N ₂ H ₄	32,048	95,186	236,651	-25,3185	8,3608
22	C	12,011	715,003	157,853	6,4461	1,9977
23	CH	13,019	594,128	182,723	2,4421	3,,0829
24	HCN	27,027	130,540	201,631	-5,3642	4,6367



Annex



Properties of Gases

		M_i [kg/kmol]	$h_{i,m,ref}$ [kJ/mol]	$s_{i,m,ref}$ [kJ/mol K]	$\pi_{A,i}$	$\pi_{B,i}$
25	HCNO	43,027	-116,733	238,048	-10,1563	6,0671
26	HCO	29,019	-12,133	224,421	-,2313	4,2667
27	CH ₂	14,027	385,220	180,882	-5,6013	4,2667
28	CH ₂ O	30,027	-115,896	218,496	-8,5350	5,4012
29	CH ₃	15,035	145,686	193,899	-10,7155	5,3026
30	CH ₂ OH	31,035	-58,576	227,426	-15,3630	6,6590
31	CH ₄	16,043	-74,873	185,987	-17,6257	6,1658
32	CH ₃ OH	32,043	-200,581	240,212	-18,7088	7,3989
33	CO	28,011	-110,529	197,343	4,0573	3,1075
34	CO ₂	44,011	-393,522	213,317	-5,2380	4,8586
35	CN	26,019	456,056	202,334	4,6673	3,1075
36	C ₂	24,022	832,616	198,978	1,9146	3,5268



Annex



Properties of Gases

		M_i [kg/kmol]	$h_{i,m,ref}$ [kJ/mol]	$s_{i,m,ref}$ [kJ/mol K]	$\pi_{A,i}$	$\pi_{B,i}$
37	C ₂ H	25,030	476,976	207,238	-4,6242	4,6367
38	C ₂ H ₂	26,038	226,731	200,849	-15,3457	6,1658
39	C ₂ H ₃	27,046	279,910	227,861	-17,0316	6,9056
40	CH ₃ CO	43,046	-25,104	259,165	-24,2225	8,5334
41	C ₂ H ₄	28,054	52,283	219.,468	-26,1999	8,1141
42	CH ₃ COH	44,054	-165,979	264.061	-30,7962	9,6679
43	C ₂ H ₅	29,062	110,299	228,183	-32,6833	9,2980
44	C ₂ H ₆	30,070	-84,667	228,781	-40,4718	10,4571
45	C ₃ H ₈	44,097	-103,847	269,529	-63,8077	14,7978
46	C ₄ H ₂	50,060	465,679	250,437	-34,0792	10,0379
47	C ₄ H ₃	51,068	455,847	273,424	-36,6848	10,8271
48	C ₄ H ₈	56,108	16,903	295,298	-72,9970	16,7215



Properties of Gases

		M_i [kg/kmol]	$h_{i,m,ref}$ [kJ/mol]	$s_{i,m,ref}$ [kJ/mol K]	$\pi_{A,i}$	$\pi_{B,i}$
49	C ₄ H ₁₀	58,124	-134,516	304,850	-86,8641	19,0399
50	C ₅ H ₁₀	70,135	-35,941	325,281	-96,9383	20,9882
51	C ₅ H ₁₂	72,151	-160,247	332,858	-110,2702	23,3312
52	C ₆ H ₁₂	84,152	-59,622	350,087	-123,2381	25,5016
53	C ₆ H ₁₄	86,178	-185,560	380,497	-137,3228	28,2638
54	C ₇ H ₁₄	98,189	-72,132	389,217	-147,4583	29,6956
55	C ₇ H ₁₆	100,205	-197,652	404,773	-162,6188	32,6045
56	C ₈ H ₁₆	112,216	-135,821	418,705	-173,7077	34,5776
57	C ₈ H ₁₈	114,232	-223,676	430,826	-191,8158	37,6111
58	C ₂ H ₄ O	44,054	-51,003	243,044	-34,3705	
59	HNO ₃	63,016	-134,306	266,425	-19,5553	
60	He	4,003	0,000	125,800		



Enthalpies of Alkanes

Alkane	$\Delta H^\circ_{\text{exp}}$	$\Delta H^\circ_{\text{calcd}}$	$ \Delta $	Alkane	$\Delta H^\circ_{\text{exp}}$	$\Delta H^\circ_{\text{calcd}}$	$ \Delta $
<i>n</i> -Pentane	-41.36	-41.41	0.05	2-Methylheptane	-60.98	-60.96	0.02
<i>n</i> -Hexane	-47.52	-47.51	0.01	3-Methylheptane	-60.34	-60.34	0.00
<i>n</i> -Heptane	-53.63	-53.62	0.01	4-Methylheptane	-60.17	-60.17	0.00
<i>n</i> -Octane	-59.74	-59.73	0.01	3-Ethylhexane	-59.88	-59.88	0.00
<i>n</i> -Nonane	-65.84	-65.84	0.00	5-Methylnonane	-74.28	-74.28	0.00
<i>n</i> -Decane	-71.95	-71.94	0.01	2-Methylnonane	-74.74	-74.74	0.00
<i>n</i> -Undecane	-78.06	-78.05	0.01	2,2-Dimethylbutane	-51.00	-51.01	0.01
<i>n</i> -Dodecane	-84.16	-84.16	0.00	2,3-Dimethylbutane	-49.48	-49.55	0.07
<i>n</i> -Tridecane	-90.27	-90.27	0.00	2,2-Dimethylpentane	-57.05	-57.06	0.01
<i>n</i> -Tetradecane	-96.38	-96.37	0.01	2,3-Dimethylpentane	-55.81	-55.81	0.00
<i>n</i> -Pentadecane	-102.49	-102.48	0.01	2,4-Dimethylpentane	-56.17	-56.17	0.00
<i>n</i> -Cetane	-108.58	-108.59	0.01	3,3-Dimethylpentane	-56.07	-56.05	0.02
<i>n</i> -Heptadecane	-114.69	-114.70	0.01	2,2-Dimethylhexane	-62.63	-62.63	0.00
<i>n</i> -Octadecane	-120.80	-120.80	0.00	2,3-Dimethylhexane	-60.40	-60.42	0.02
<i>n</i> -Nonadecane	-126.90	-126.91	0.01	2,4-Dimethylhexane	-61.47	-61.44	0.03
<i>n</i> -Eicosane	-133.01	-133.02	0.01	2,5-Dimethylhexane	-62.26	-62.21	0.05
2-Methylbutane	-42.85	-42.82	0.03	3,3-Dimethylhexane	-61.58	-61.56	0.02
2-Methylpentane	-48.82	-48.87	0.05	3,4-Dimethylhexane	-60.23	-60.23	0.00
3-Methylpentane	-48.28	-48.30	0.02	2-Methyl-3-ethylpentane	-59.69	-59.68	0.01
2-Methylhexane	-54.93	-54.92	0.01	3-Methyl-3-ethylpentane	-60.46	-60.48	0.02
3-Methylhexane	-54.35	-54.34	0.01	3,3-Diethylpentane	-65.84	-65.84	0.00
3-Ethylpentane	-53.77	-53.77	0.00				



Annex



Rx of Formation	Standard Enthalpy of Formation Table
	$\Delta H_{\text{formation}}$
	Substance kJ/mol
Al(s) → Al(s)	0
Al(s) + 3/2 O ₂ (g) → Al ₂ O ₃ (s)	-1670
C(s, graphite) → C(s, graphite)	0
C(s) + 1/2 O ₂ (g) → CO(g)	-111
C(s) + O ₂ (g) → CO ₂ (g)	-394
C(s) + 2H ₂ (g) → CH ₄ (g)	-75
C(s) + 2H ₂ (g) + 1/2 O ₂ (g) → CH ₃ OH(l)	-239
2C(s) + H ₂ (g) → C ₂ H ₂ (g)	227
2C(s) + 2H ₂ (g) → C ₂ H ₄ (g)	52
2C(s) + 3H ₂ (g) → C ₂ H ₆ (g)	-85
2C(s) + 3H ₂ (g) + 1/2 O ₂ (g) → C ₂ H ₅ OH(l)	-278
Ca(s) + 1/2 O ₂ (g) → CaO(s)	-636
Ca(s) + O ₂ (g) + H ₂ (g) → Ca(OH) ₂ (s)	-987
Ca(s) + S(s) + 2O ₂ (g) → CaSO ₄ (s)	-1433
Cl ₂ (g) → Cl ₂ (g)	0
2Fe(s) + 3/2 O ₂ (g) → Fe ₂ O ₃ (s)	-822
H ₂ (g) → H ₂ (g)	0
1/2 H ₂ (g) + 1/2 Cl ₂ (g) → HCl(g)	-92
H ₂ (g) + 1/2 O ₂ (g) → H ₂ O(g)	-242
H ₂ (g) + 1/2 O ₂ (g) → H ₂ O(l)	-286
H ₂ (g) + O ₂ (g) → H ₂ O ₂ (l)	-188
1/2 H ₂ (g) + S(s) → H ₂ S(g)	-20
H ₂ (g) + S(s) + 2O ₂ (g) → H ₂ SO ₄ (l)	-811
Hg(l) → Hg(l)	0
Hg(l) → Hg(g)	61
Mg(s) + 1/2 O ₂ (g) → MgO(s)	-602
N ₂ (g) → N ₂ (g)	0
1/2 N ₂ (g) + 3/2 H ₂ (g) → NH ₃ (g)	-46
1/2 N ₂ (g) + 2H ₂ (g) + 1/2 Cl ₂ (g) → NH ₄ Cl(s)	-315
N ₂ (g) + 1/2 O ₂ (g) → N ₂ O(g)	82
N ₂ (g) + 2O ₂ (g) → N ₂ O ₄ (g)	10
Na(s) + 1/2 Cl ₂ (g) → NaCl(s)	-411
Na(s) + 1/2 O ₂ (g) + 1/2 H ₂ (g) → NaOH(s)	-427
O ₂ (g) → O ₂ (g)	0
4P(s) + 5O ₂ (g) → P ₂ O ₁₀ (s)	-2980
S(s) → S(s)	0
S(s) + O ₂ (g) → SO ₂ (g)	-297
S(s) + 3/2 O ₂ (g) → SO ₃ (g)	-395

ΔH_f° (kJ/mol) (concentration of aqueous solutions is 1M)					
Substance	ΔH_f°	Substance	ΔH_f°	Substance	ΔH_f°
Ag(s)	0	CsCl(s)	-443.04	H ₃ PO ₄ (aq)	-1279.0
AgCl(s)	-127.068	Cs ₂ SO ₄ (s)	-1443.02	H ₂ S(g)	-20.63
AgCN(s)	146.0	CuI(s)	-67.8	H ₂ SO ₃ (aq)	-608.81
Al ₂ O ₃	-1675.7	CuS(s)	-53.1	H ₂ SO ₄ (aq)	-814.0
BaCl ₂ (aq)	-871.95	Cu ₂ S(s)	-79.5	HgCl ₂ (s)	-224.3
BaSO ₄	-1473.2	CuSO ₄ (s)	-771.36	Hg ₂ Cl ₂ (s)	-265.22
BeO(s)	-609.6	F ₂ (g)	0	Hg ₂ SO ₄ (s)	-743.12
C(s) + 2H ₂ (g) → CH ₄ (g)	-75	BiCl ₃ (s)	-399.49	I ₂ (s)	0
C(s) + 2H ₂ (g) + 1/2 O ₂ (g) → CH ₃ OH(l)	-239	FeO(s)	-272.0	K(s)	0
2C(s) + H ₂ (g) → C ₂ H ₂ (g)	227	FeS(s)	-100.0	KBr(s)	-393.798
2C(s) + 2H ₂ (g) → C ₂ H ₄ (g)	52	Fe ₂ O ₃ (s)	-824.2	KMnO ₄ (s)	-837.2
2C(s) + 3H ₂ (g) → C ₂ H ₆ (g)	-85	Fe ₃ O ₄ (s)	-1118.4	KOH	-424.764
2C(s) + 3H ₂ (g) + 1/2 O ₂ (g) → C ₂ H ₅ OH(l)	-278	H(g)	217.965	LiBr(s)	-351.213
Ca(s) + 1/2 O ₂ (g) → CaO(s)	-636	H ₂ (g)	0	LiOH(s)	-484.93
Ca(s) + O ₂ (g) + H ₂ (g) → Ca(OH) ₂ (s)	-987	HBr(g)	-36.40	Mn(s)	0
Ca(s) + S(s) + 2O ₂ (g) → CaSO ₄ (s)	-1433	HCl(g)	-92.307	MnCl ₂ (aq)	-555.05
Cl ₂ (g) → Cl ₂ (g)	0	HCl(aq)	-167.159	Mn(NO ₃) ₂ (aq)	-635.5
2Fe(s) + 3/2 O ₂ (g) → Fe ₂ O ₃ (s)	-822	HCN(aq)	108.9	MnO ₂ (s)	-520.03
H ₂ (g) → H ₂ (g)	0	HCHO	-108.57	MnS(s)	-214.2
1/2 H ₂ (g) + 1/2 Cl ₂ (g) → HCl(g)	-92	HCOOH(l)	-424.72	N ₂ (g)	0
H ₂ (g) + 1/2 O ₂ (g) → H ₂ O(g)	-242	HF(g)	-271.1	NH ₃ (g)	-46.11
H ₂ (g) + 1/2 O ₂ (g) → H ₂ O(l)	-286	HI(g)	26.48	NH ₄ Br(s)	-270.83
H ₂ (g) + O ₂ (g) → H ₂ O ₂ (l)	-188	H ₂ O(l)	-285.830	NO(g)	90.25
1/2 H ₂ (g) + S(s) → H ₂ S(g)	-20	Co ₃ O ₄ (s)	-891	NO ₂ (g)	33.18
H ₂ (g) + S(s) + 2O ₂ (g) → H ₂ SO ₄ (l)	-811	CoO(s)	-237.94	N ₂ O(g)	82.05
Hg(l) → Hg(l)	0	Cr ₂ O ₃ (s)	-1139.7	H ₃ PO ₄ (l)	0
Hg(l) → Hg(g)	61			Na(s)	0
Mg(s) + 1/2 O ₂ (g) → MgO(s)	-602				
N ₂ (g) → N ₂ (g)	0				
1/2 N ₂ (g) + 3/2 H ₂ (g) → NH ₃ (g)	-46				
1/2 N ₂ (g) + 2H ₂ (g) + 1/2 Cl ₂ (g) → NH ₄ Cl(s)	-315				
N ₂ (g) + 1/2 O ₂ (g) → N ₂ O(g)	82				
N ₂ (g) + 2O ₂ (g) → N ₂ O ₄ (g)	10				
Na(s) + 1/2 Cl ₂ (g) → NaCl(s)	-411				
Na(s) + 1/2 O ₂ (g) + 1/2 H ₂ (g) → NaOH(s)	-427				
O ₂ (g) → O ₂ (g)	0				
4P(s) + 5O ₂ (g) → P ₂ O ₁₀ (s)	-2980				
S(s) → S(s)	0				
S(s) + O ₂ (g) → SO ₂ (g)	-297				
S(s) + 3/2 O ₂ (g) → SO ₃ (g)	-395				

ΔH_f° / kJ mol ⁻¹					
H ₂ O(l)	-286	NO ₂ (g)	+33	CH ₄ (g)	-75
H ₂ O(g)	-242	N ₂ O ₄ (g)	+9	C ₂ H ₆ (g)	-85
CO(g)	-111	CaO(s)	-635	C ₂ H ₄ (g)	+52
CO ₂ (g)	-394	CaCO ₃ (s)	-1207	C ₂ H ₂ (g)	+227
HCl(g)	-92	Fe ₂ O ₃ (s)	-824	C ₂ H ₅ OH(l)	-278
NH ₃ (g)	-46	NaCl(s)	-411	C ₆ H ₆ (l)	+49
NO(g)	+90	BaSO ₄ (s)	-1473	CH ₂ O(g)	-109

Transport Coefficients

Momentum

$$\eta_{ij} = 266.93 \cdot 10^{-8} \left(\frac{\sqrt{2M_i M_j T / (M_i + M_j)}}{\sigma_{ij}^2 \Omega_{ij}^{(2,2)*}(T_{ij}^*)} \right);$$

Heat

$$\lambda_{ij} = 8.3 \cdot 10^{-4} \left(\frac{\sqrt{T(M_i + M_j) / 2M_i M_j}}{\sigma_{ij}^2 \Omega_{ij}^{(2,2)*}(T_{ij}^*)} \right);$$

Mass

$$D_{ij} = 26.28 \cdot 10^{-8} \left(\frac{\sqrt{T^3 (M_i + M_j) / 2M_i M_j}}{p \sigma_{ij}^2 \Omega_{ij}^{(1,1)*}(T_{ij}^*)} \right)$$

Already rather complex but this is for binary mixtures only, for multi-component mixtures no general analytical solution exists.

Transport Coefficients

Collision integrals

$$\Omega^{(l,s)*}(T) = \frac{1}{(s+1)!} \int_0^\infty \exp(-E/T) \left(\frac{E}{T}\right)^{s+1} Q^{(l)*}(E) d\left(\frac{E}{T}\right),$$

$$Q^{(l)*}(E) = \frac{1}{\left(1 - \frac{1 + (-1)^l}{2(1+l)}\right)} \int_0^\infty (1 - \cos^l \chi) b db,$$

$$\chi(E, b) = \pi - 2b \int_{r_m}^\infty \frac{dr}{r^2 \sqrt{1 - \frac{\varphi(r)}{E} - \frac{b^2}{r^2}}}$$

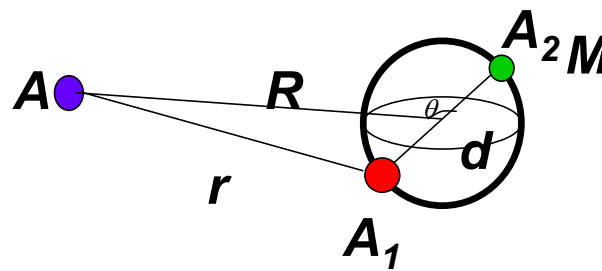


However, the interaction potential $\phi(r)$ is still unknown and therefore approximations (functions) based on experiments with adjustable constants are used.

Interaction potential $\varphi_{ij}(r)$

Method of Addition (represent physico-chemical properties of molecule by sum of its structural elements)

$$\varphi(R, \theta)_{A-M} = \sum_i \varphi(r)_{A-A_i^M}$$



Example for two linear molecules:

$$\Phi(r, \vec{d}_1, \vec{d}_2) = \sum_i^{n_1} \sum_j^{n_2} \langle \varphi_{ij}(R) \rangle$$

$$\langle \varphi_{ij}(R) \rangle = \frac{1}{16\pi^2} \int_0^\pi \int_0^{2\pi} \sin \theta_2 d\theta_2 d\phi_2 \int_0^\pi \int_0^{2\pi} \varphi_{ij} [r_{ij}(R, d_{1i}, d_{2j}, \theta_1, \theta_2, (\phi_1 - \phi_2))] \sin \theta_1 d\theta_1 d\phi_1$$